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**Abstract.** High-resolution optical coherence tomography (OCT) retinal imaging is important to noninvasively visualize the various retinal structures to aid in better understanding of the pathogenesis of vision-robbing diseases. However, conventional OCT systems have a trade-off between lateral resolution and depth-of-focus. In this report, we present the development of a focus-stacking OCT system with automatic focus optimization for high-resolution, extended-focal-range clinical retinal imaging by incorporating a variable-focus liquid lens into the sample arm optics. Retinal layer tracking and selection was performed using a graphics processing unit accelerated processing platform for focus optimization, providing real-time layer-specific *en face* visualization. After optimization, multiple volumes focused at different depths were acquired, registered, and stitched together to yield a single, high-resolution focus-stacked dataset. Using this system, we show high-resolution images of the retina and optic nerve head, from which we extracted clinically relevant parameters such as the nerve fiber layer thickness and lamina cribrosa microarchitecture. © 2016 Society of Photo-Optical Instrumentation Engineers (SPIE) [DOI: 10.1117/1.JBO.21.2.026007]

**Keywords:** high-resolution optical coherence tomography; focus-stacking; variable-focus lens; *en face* optical coherence tomography; graphics processing unit acceleration.

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## 1 Introduction

High-resolution visualization of the retinal morphology can assist ophthalmologists to better understand the pathogenesis of retinal diseases. In glaucoma, for example, studies on non-human primates have indicated that morphological changes in the lamina cribrosa may precede the degeneration of retinal ganglion cell axons.<sup>1-3</sup> Similarly, changes in the density of the photoreceptor mosaic are associated with functional vision loss and retinal degeneration.<sup>4,5</sup>

Optical coherence tomography (OCT) provides cross-sectional images of the retina with exquisite axial resolution, and is commonly used in ophthalmology. In OCT, the axial resolution is determined by the source spectrum, whereas the lateral resolution is determined by the numerical aperture (NA) of the sample arm. For retinal OCT imaging, the cornea and lens act as the imaging objective, so the beam diameter at the pupil determines the NA and hence the focused spot size at the retina. Clinical OCT systems operating at an 830-nm center wavelength commonly use a beam diameter of  $\sim 1$  mm at the cornea, corresponding to a lateral resolution on the order of  $\sim 20$   $\mu\text{m}$  at the retina. This resolution is approximately one order of magnitude worse than the theoretical best axial OCT resolution, which is on the order of  $\sim 1$  to  $2$   $\mu\text{m}$ . By increasing the probe beam diameter at the cornea, the lateral resolution can be (in principle) improved, but this approach reduces the depth-of-focus as a trade-off. Since imaging through the entire thickness of the retina and structures of the optic nerve head (ONH) is desirable, high lateral resolution with short depth-of-focus

may not be suitable in the clinical environment. Therefore, an extended depth-of-focus imaging system capable of maintaining high lateral resolution within the layers of interest is important. Many methods have been proposed in the literature to overcome this axial depth limitation. These methods include mechanical motion of the sample arm,<sup>6</sup> the addition of focus-modulating elements, such as acousto-optic tunable lenses and axicon lenses, and adaptive optics.<sup>7-10</sup> Multibeam systems have also been reported.<sup>11</sup> Computational approaches such as interferometric synthetic aperture microscopy<sup>12,13</sup> and the Gabor-based fusion technique with dynamic focus using liquid lens<sup>14</sup> have also been successfully used to correct for defocus in postprocessing and provide axial focus extension.

In this paper, we describe an autofocus and high-speed swept-source (SS) OCT imaging system for acquiring *in vivo* high-resolution images of the entire retinal structure and ONH using a focus-stacking method. Since recent developments in SS-OCT engines have resulted in longer imaging depths as compared with spectral domain-OCT (SD-OCT) systems,<sup>15</sup> the entire thickness of the retina can be visualized even with a high-NA sample arm. However, a tightly focused spot reduces the intensity in the regions outside the focal depth. Similarly, high lateral resolution imaging is limited to the depth-of-focus. In order to overcome these limitations, in this study, a commercially available variable-focus liquid lens was incorporated into an SS-OCT system, and controlled by a graphics processing unit (GPU)-based data acquisition platform. In the GPU-based real-time autofocus processing algorithm/pipeline, focus optimization was performed at a user-specified layer and facilitated by real-time axial tracking to extract the same

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retinal layer throughout the optimization process. Following the optimization, multiple volumes at different focal depths in the retina were successively acquired. In order to achieve high lateral resolution throughout the imaging depth, Gaussian-weighted averaging was applied to the focus-stacked volumes, permitting visualization of the retina along the entire axial extent with high resolution. We demonstrated imaging of the entire three-dimensional (3-D) morphology of the ONH *in vivo*, from which we can study the morphological changes in the nerve fiber layer (NFL) and lamina cribrosa due to diseases such as glaucoma.<sup>16–21</sup> The system is compact in size and capable of imaging the human retina with sufficiently large field of view, which complements our on-going clinical studies.<sup>17,22</sup>

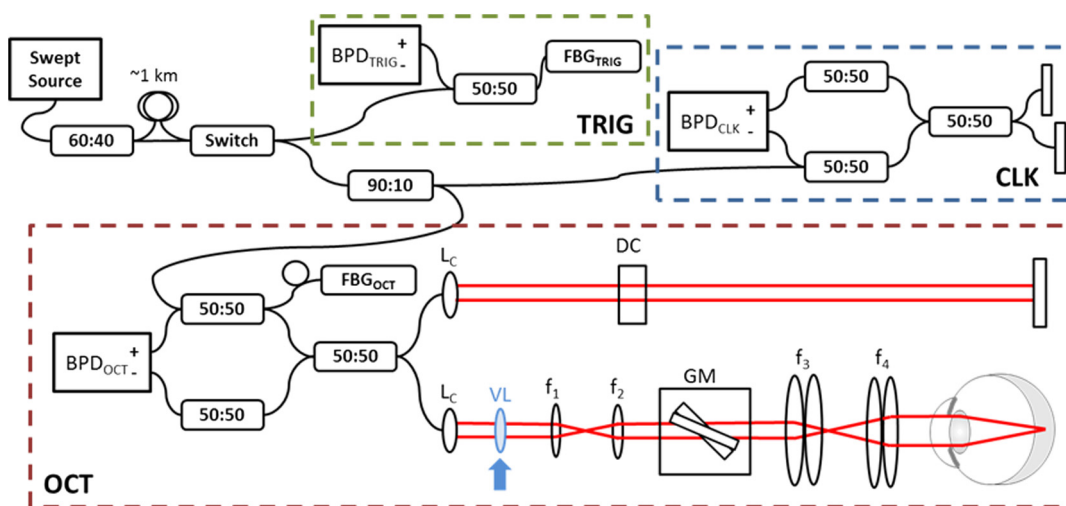
The remainder of this report is organized as follows: we first describe the optical design of our SS-OCT acquisition system. We next describe our custom-written GPU-accelerated retinal tracking and focus optimization algorithm that provided real-time *en face* visualization. The retinal tracking was combined with a simple but rapid segmentation algorithm that provided the metric for layer-specific focusing during optimization, as well as real-time feedback during the optimization process to the user. Last, we describe the acquisition and processing steps used to generate a focus-stacked dataset, and present images acquired from human volunteers.

## 2 Methods

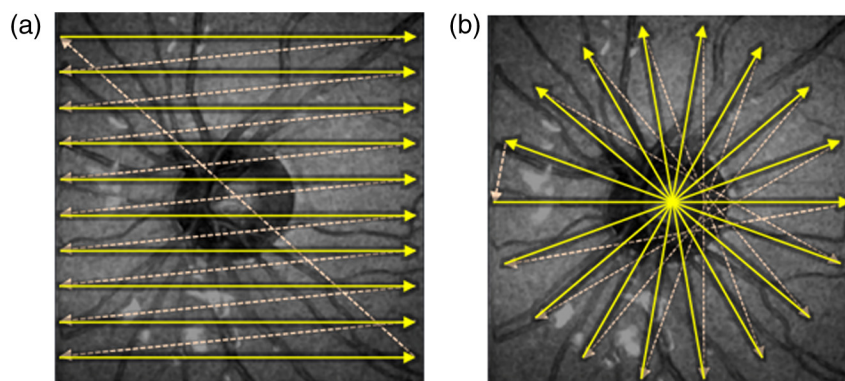
In order to demonstrate the clinical utility of the system, the posterior eye chamber of human volunteers without any remarkable retinal disorder were imaged. All protocols for measurement were approved by the Office for Research Ethics at Simon Fraser University. Written and informed consent was obtained prior to imaging. Figure 1 shows the schematic of our custom-built 1060-nm swept-source OCT system. A wavelength swept laser (Axsun Technologies, Massachusetts) with a scanning frequency of 100 kHz, a center wavelength of 1060 nm and a full width half maximum (FWHM) of 85 nm was used as a light source. The swept laser had a duty cycle of around

66% and hence has a dead time between the wavelength scans of approximately  $3.6\ \mu\text{s}$ . In order to increase the A-scan rate from 100 kHz to 200 kHz, we implemented a “double-buffered configuration.”<sup>23</sup> The swept-source output was split into original and buffered fiber paths by a 60:40 fiber coupler, with 60% of the optical power route to the buffered path. A single-mode fiber spool of  $\sim 1\ \text{km}$  (HI1060, Corning, New York) was placed in the buffered path to create a delay of  $\sim 5\ \mu\text{s}$  between the two paths. The original and buffered paths were recombined using a fast optical switch (Nanona Optical Switch, Boston Applied Technologies, Inc., Massachusetts) that had a switch time of  $<60\ \text{ns}$  and a maximum cross-talk suppression of 26 dB.<sup>24</sup> The switch output was split 90:10, with 90% of the power going to the OCT system, and the other 10% going to the k-clock calibration signal. The switch was controlled using a 100-kHz square wave signal that was generated using the data acquisition card (National Instruments, Texas) and synchronized to the A-scan trigger provided by the swept-source laser. The duty cycle of the swept-source engine was over 50%; however, by tuning the timing of the square wave signal, we were able to preserve the portion of the spectrum with the greatest intensity. The double-buffered spectrum had a reduced FWHM bandwidth of 75 nm, corresponding to an estimated coherence length of  $\sim 6.6\ \mu\text{m}$  (in air). A Fiber-Bragg grating (FBG, OE Land, Quebec, Canada,  $\lambda_c = 985.17\ \text{nm}$ ,  $\Delta\lambda = 0.08\ \text{nm}$ , reflectivity = 99.16%) was connected to the other port of the switch to generate the A-scan trigger. This FBG was designed to reflect a narrow wavelength band located near the beginning of the spectrum, outside of the 3-dB bandwidth. In Fig. 1, a schematic of the double-buffered source and its connections to the A-scan trigger, k-clock, and OCT system is presented.

The OCT interferometer consisted of three wavelength-flattened couplers in a balanced configuration. A variable-focus lens (VL; ARCTIC 316-AR850, Lyon, France) was added to dynamically adjust the focus of the OCT beam to a user-selected retinal layer. The VL had a dynamic range of 18 diopters ( $-5\ \text{D}$



**Fig. 1** Schematic of double-buffered 200-kHz SS-OCT system, including the A-scan trigger (TRIG), sampling clock (CLK), and OCT system (OCT). A variable-focus liquid lens (VL) was included in the sample arm to provide dynamic focus adjustment. The sample arm consisted of two telescopes that relayed the conjugate plane from the VL to the scanning mirror and pupil. DC: dispersion compensation; BPD: balanced photo-diode detector; FBG: Fiber-Bragg grating; GM: galvanometer-scanning mirror;  $L_c$ : collimating lens.



**Fig. 2** (a) Raster and (b) radial scanning protocols. Radial scan was adopted for regions that exhibited radial symmetry, and required denser sampling in the center relative to the periphery.

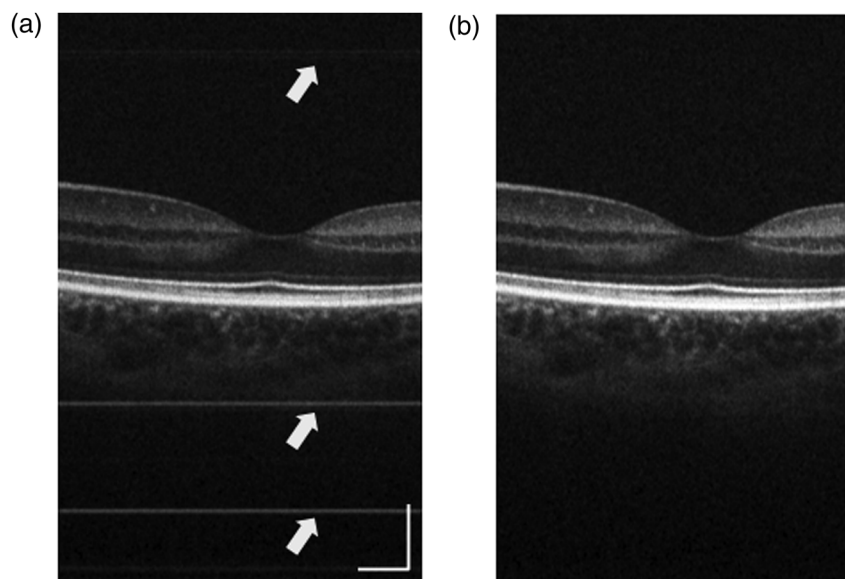
to +13 D), which resulted in an ocular diopter shift of 29 D (−9 to 20 D). Two telescopes were placed between the VL and ocular pupil to relay the VL, galvanometer-scanning mirrors, and pupil on conjugate planes. The sample arm delivered a 3.0-mm ( $1/e^2$  diameter) beam to the pupil, resulting in a calculated  $\sim 4.3\text{-}\mu\text{m}$  spot size (FWHM) with  $\sim 120\text{-}\mu\text{m}$  depth-of-focus (calculated as twice the Rayleigh range) at the retina.

### 2.1 Optical Coherence Tomography Image Acquisition, Segmentation, A-scan Alignment, and Optimization

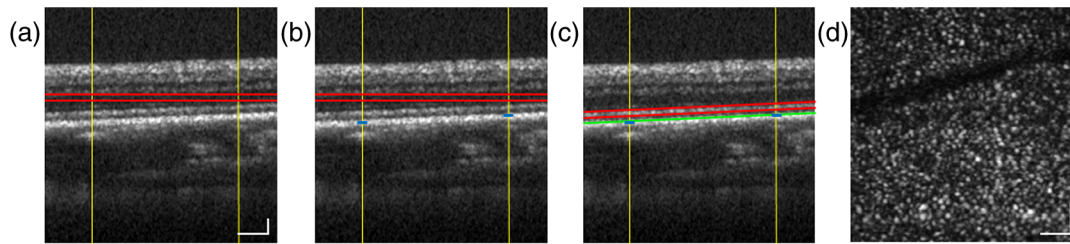
Figure 2 shows two different scanning protocols used for the volume acquisition. For the conventional approach shown in Fig. 2(a), we used a raster scan pattern with 80% duty cycle. Each acquired volume consisted of  $400 \times 400$  A-scans, which resulted in an acquisition rate of 1 volume/s. A radial scan approach [Fig. 2(b)] was adopted for regions that exhibited centro-symmetry, such as the ONH. In these regions, dense sampling was desirable near the center, whereas sparser-sampling was acceptable near the periphery. For radially acquired data, 180 to 300 B-scans per volume were acquired evenly spaced in

angle, with 600 A-scans per B-scan. Each volume took 0.8 to 1.2 s to acquire.

Our open-sourced GPU-accelerated FD-OCT acquisition code was modified for this project.<sup>25–27</sup> For this work, the GPU used was a GeForce GTX Titan (NVIDIA, Santa Clara, California) that provided a 1024-pt A-scan processing rate of 4 MHz, which is significantly faster than the data acquisition rate, and thus permitting computational bandwidth for additional processing. The phase instability caused by fluctuations in the synchronization between the wavelength sweep of the light source and digitizer trigger signal resulted in undesirable horizontal-line artifacts in the B-scans, which degraded the image quality and potentially interfered with the retinal axial tracking algorithm. Figure 3 shows the B-scan OCT image before (a) and after (b) stabilizing the phase of OCT signal. In the stabilization process, the artifacts appearing as horizontal lines in Fig. 3(a) were removed in real-time on the GPU by aligning each A-scan to a reference wave number that was provided by the FBG (OE Land, QC, Canada,  $\lambda_c = 988.81$  nm,  $\Delta\lambda = 0.05$  nm, reflectivity = 93.15%) in the OCT interferometer (Fig. 1).<sup>28</sup>



**Fig. 3** DC line artifacts due to A-scan misalignments. (a) The DC line artifact is shown with an arrow before the alignment. (b) Alignment of A-scans removed the artifact. Scale bars denote  $250\ \mu\text{m}$ .



**Fig. 4** Simple segmentation algorithm for real-time axial tracking and *en face* visualization. (a) The user manually selected the thickness of *en face* layer (red lines) and two a-scans for segmentation (yellow lines). (b) The algorithm detected the maximum-intensity pixel at each location (blue bars). (c) The location of the brightest layer in the retina (green line) was interpolated from the two maximum-intensity pixels (blue bars). This location was then used to determine the tilt in the other *en face* layers. (d) The *en face* image was generated by summing up the pixels within the two red lines. The image was taken at an eccentricity of  $\sim 6$  deg from the fovea. Scale bars denote  $50\ \mu\text{m}$ .

A simple segmentation algorithm was implemented in the GPU processing platform to provide real-time axial tracking of the retinal position, which changed due to patient motion, and display of *en face* images from specific layers during acquisition (Fig. 4). The algorithm tracked the relative position of the brightest layer in the retina to remove the effects of axial motion from the *en face* image. The user selected the thickness of the *en face* layer of interest (indicated by red lines), as well as two reference A-scan positions on the retina (indicated by yellow lines) to be used for tracking [Fig. 4(a)]. At each reference position, the algorithm determined the pixel with the maximum intensity (indicated by the short blue lines), and used the coordinates to determine the degree of retinal tilt (if present) as shown in Figs. 4(b) and 4(c). During acquisition, the user could dynamically adjust the axial offset between the selected layer and brightest layer to display different retinal layers in *en face* projection view shown in Fig. 4(d).

An optimization algorithm was also developed to provide automated focusing on specific layers. The optimization had a multipass approach, starting with a large search range, and then fine-tuning the search range in successive passes. The brightness of the selected layer was used as the metric for optimization. In the first pass, the optimization algorithm applied seven different ocular diopter values within a 5-D to 7-D range and recorded the resultant brightness at the specified layer. In the subsequent passes, the algorithm tested a narrower range around the diopter value that gave the maximum intensity in the previous round. For each diopter shift, 10 stationary B-scans/volumes were acquired and used to determine the summed intensity within the selected *en face* region. Thus, we had an optimization rate of 25 Hz/step, and the entire optimization process took approximately 1 s.

## 2.2 Focus-Stacking Algorithm

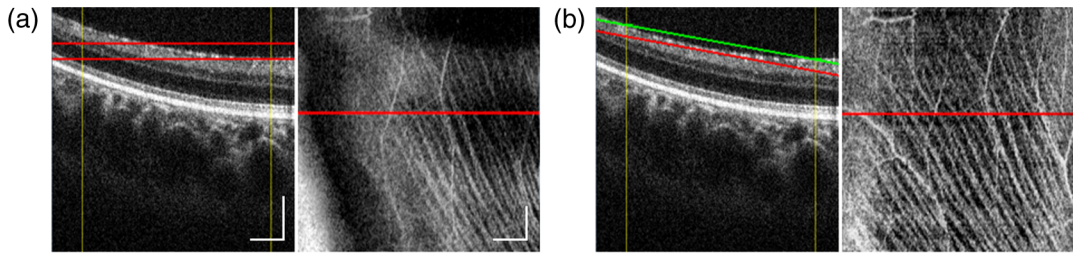
High-resolution images of the ONH structures were acquired by merging a set of focus-shifted volumes acquired using the radial scanning protocol. First, we automatically optimized the focus at the NFL and lamina cribrosa, respectively, to determine the range of diopter shifts required during acquisition. A set of 3 to 5 volumes were then acquired, with the focus shifted axially between acquisitions. The optimization algorithm steps, which included tracking, segmentation, autofocus, and tilt measurement, were performed on the same B-scan location in each volume. This pipeline was also applicable for the raster scanning acquisition protocol.

Eye motion artifacts were mitigated by using a double-buffered swept source OCT for rapid volume acquisition. However, even small motion artifacts would cause the structures in the focus-stacked volumes to mismatch. In order to compensate for the mismatches, motion correction was performed in post-processing after completing the multivolume acquisition. The relative translation between B-scans was assessed using phase correlation, and B-scan to B-scan motion registration was performed. After the two-dimensional (2-D) motion registration and conversion to Cartesian coordinates, volumetric registration was performed using the three-dimensional (3-D) rigid registration toolbox in Amira (FEI, Oregon), followed by 3-D nonrigid registration using the medical image registration toolbox.<sup>29,30</sup> For the 3-D registration, each volume in the focus-stacked dataset was registered to the previously acquired volume to maximize the amount of information overlap during the registration. After the volume registration, the A-scans within each volume were summed to determine the position of the best focus within the volume, since the depth at which the volume is focused will have greater intensity than the out-of-focus regions. From the comparison of the A-scans, the peak intensity locations are approximated so that the separations between the peaks are evenly spaced. A set of Gaussian masks were automatically generated at the approximated focus locations and normalized to perform weighted averaging, which resulted in a high-resolution volume of the entire ONH.<sup>31</sup>

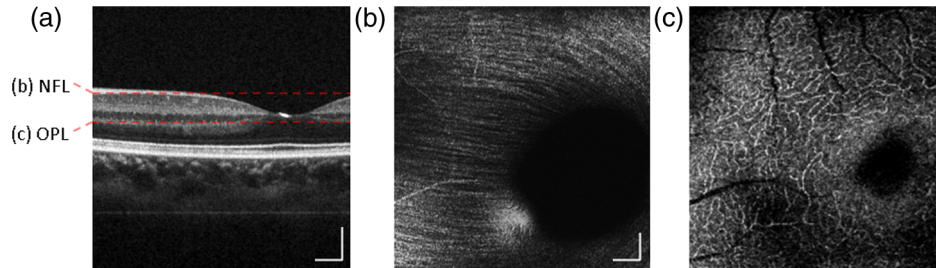
## 3 Results

Figure 5 shows the *en face* views generated using our segmentation and *en face* display code, as presented in real-time during acquisition. The B-scans were also included to show the results of the segmentation, and the thickness and location of the *en face* layer. In the *en face* image generated from the segmented B-scans, the nerve fiber bundles are clearly visualized. In comparison, without segmentation, artifacts from retinal tilt and axial motion degrade the *en face* image, and the resultant *en face* view is not from a single layer, but is instead a contribution from multiple layers.

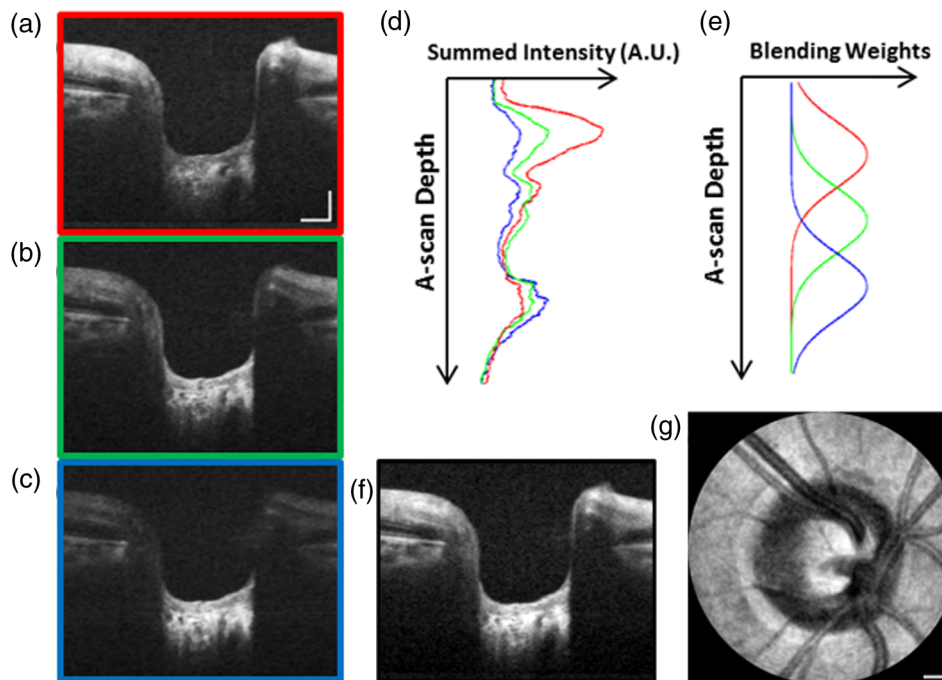
Figure 6 shows representative *en face* images of the NFL (b) and the outer plexiform layer (OPL) (c), with the focus automatically optimized at the corresponding layer marked by red-dashed lines in the B-scan OCT image (a). The high resolution of the system permitted visualization of the nerve fiber bundles in the retinal NFL, and the capillary network of the OPL with high contrast.



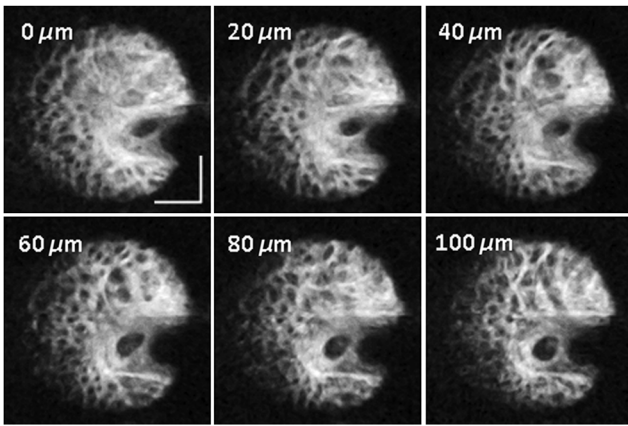
**Fig. 5** Real-time *en face* visualization (a) without and (b) with retinal tracking and anatomically based segmentation on a volume acquired using a raster scanning method. Scale bar denotes  $250\ \mu\text{m}$ .



**Fig. 6** *En face* images acquired using a raster scanning method with (a) focus on the (b) NFL and (c) microvasculature of the OPL. Scale bar denotes  $200\ \mu\text{m}$ .



**Fig. 7** Focus-stacking processing and results, acquired using a radial scanning method. (a)–(c) A set of volumes focused at different depths, from the NFL (a) to the lamina cribrosa (c) were acquired. (d) The summed A-scans from each volume are compared to determine the focused depth of each volume. For a given volume, the position of best focus will correspond to the depth at which the summed intensity is at maximum in comparison to the other volumes. (e) From the comparison of the summed A-scans, a set of Gaussian masks are generated to perform weighted-averaging of the volumes. (f) Each B-scan from (a)–(c) is stitched together. Representative B-scan from the focus-stacked volume shows uniformly high resolution across the entire extent. (g) The stitched results showing the focus-stacked dataset. The entire ONH region is in focus, in comparison to the originally acquired data sets. Scale bars denote  $200\ \mu\text{m}$ .



**Fig. 8** Depth-resolved images of lamina cribrosa from a focus-stacked radially scanned volume, acquired in 20- $\mu$ m increments from the anterior surface of the lamina cribrosa. Scale bars denote 200  $\mu$ m.

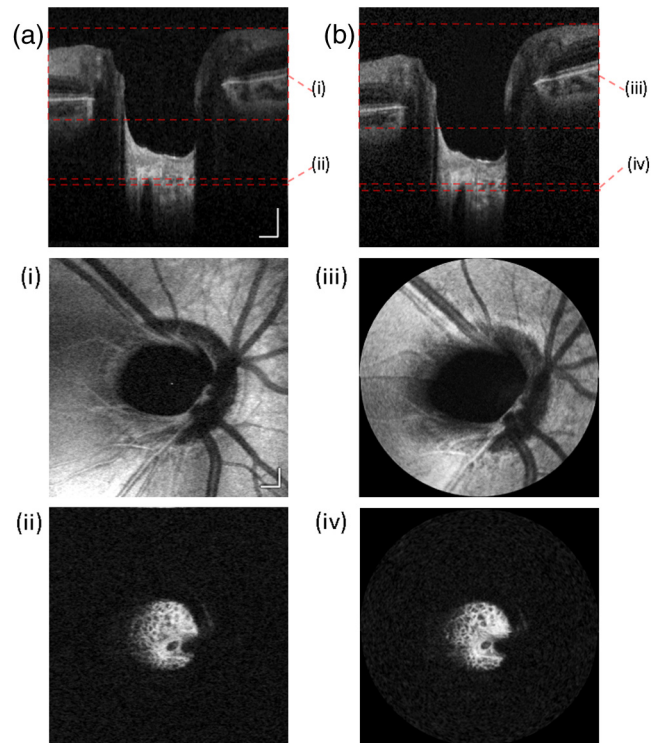
Figure 7 shows the focus-stacking result with a representative data set acquired at the ONH. In the representative B-scan OCT images shown in Figs. 7(a)–7(c), focus was set at: (a) the retinal surface, (b) the bottom of the cup, and (c) the lamina cribrosa. The summation result of A-scans within each volume set and the corresponding Gaussian masks are also shown in Figs. 7(d) and 7(e). Figures 7(f) and 7(g) are the stitched result of three different focus-stacked B-scans and the *en face* view of the focus-stacked dataset, respectively. In addition, as shown in Fig. 8, depth-resolved images of the lamina cribrosa microarchitecture can also be visualized from the focus-stacked data set.

#### 4 Discussion

We have demonstrated a focus-stacking OCT imaging system with real-time image-based axial retinal tracking and focus optimization. Using the system, we were able to image the ONH with high resolution throughout the axial extent of the structure, from which we could clearly visualize the lamina cribrosa microarchitecture as well as the inner retinal layers. Both of these parameters are important in better identifying factors that precede vision loss in glaucoma.<sup>1,17,22,32,33</sup> We also demonstrated the capability of the system in visualizing the macular microvasculature in the OPL and the pattern of nerve fiber bundles emanating from the ONH toward the macula. The ability to visualize and quantify the appearance of nerve fiber bundles traversing the retinal surface has potential as a sensitive early diagnostic biomarker.<sup>16,34,35</sup> Furthermore, we employed two scanning protocols, raster and radial scanning. Figure 9 shows a comparison between the raster (left column) and radial scan (right column) methods at the ONH. The radial scan had a reduced overall number of sampling points compared to the raster scan pattern, effectively reducing the acquisition time by ~25%. The radial scan pattern provided more densely spaced samples at the lamina cribrosa located at the center of the imaging field, whereas the outer region of the scan was under-sampled. The missing data points were reconstructed using a 2-D cubic interpolation, permitting measurements of peripapillary NFL thickness.<sup>36</sup> These centro-symmetrical high sampling characteristics make the radial scanning method more efficient in the case of imaging the ONH.

A key component of our imaging system was the GPU-accelerated real-time retinal tracking and focus optimization

algorithm, which allowed real-time *en face* visualization of a user-selected retinal layer for feedback during acquisition as well as layer-specific optimization. By performing the relevant preprocessing steps in real time, such as A-scan alignment for timing jitter removal and interframe averaging for noise reduction, we were able to successfully track the axial position of the retina using a relatively simple segmentation algorithm, permitting visualization of *en face* retinal images with meaningful correspondence to the cellular layer physiology. The real-time image-based axial tracking and segmentation also allowed us to fine-tune our optimization to focus on specific retinal layers instead of optimizing for the brightness along the entire retina. However, there are several limitations in our study. First, although the focus optimization time was reduced down to 1 s by using a GPU-based processing platform, it is still not fast enough to avoid accommodation of the eye, which could affect the optimization result and reduce the image quality. Second, the retinal tracking method based on a simple segmentation algorithm would not properly work in cases where edema, drusen, intra- or subretinal fluid distorted the shape of retina. With higher-end GPUs and/or multi-GPU configurations, more sophisticated retinal layer segmentation algorithms will be realizable in real time. The development of higher speed focus optimization algorithms and more sophisticated segmentation algorithms for robust tracking of the retina in nonideal conditions is the focus of a future study. Last, because of the limited dynamic range of the variable-focus liquid lens, as described in Sec. 2, our current system has limited capabilities in highly myopic subjects.



**Fig. 9** Comparison of (a) raster scanning (400 A-scans  $\times$  400 B-scans) and (b) radial scanning (600 A-scans  $\times$  200 B-scans) methods focused at the lamina cribrosa. Similar regions (i)–(ii) and (iii)–(iv) are selected from (a) and (b), respectively, and averaged in axial directions. The corresponding *en face* images are displayed in (i)–(iv). Scale bar denotes 200  $\mu$ m.

The diameter of the imaging beam at the subject's pupil was limited to  $\sim 3$  mm. With this imaging beam diameter, the dominant aberrations in a normal population of young subjects were defocus and astigmatism.<sup>37</sup> In this work, we demonstrated the ability to track and optimize the image quality based on defocus; however, these techniques are equally applicable to astigmatism. Liquid lenses capable of correcting both defocus and astigmatism are approaching commercial availability, but a prototype was not available for demonstration at the time of this work. We have selected the 3-mm imaging beam diameter because it permits an optical design of the sample arm that provides high resolution over a clinically valuable wide field of view.

Recently, we demonstrated a wavefront sensorless adaptive optics spectral domain OCT (WSAO-SD-OCT) system for *in vivo* human retinal imaging.<sup>17,22</sup> With the GPU-based data acquisition and processing, real-time cellular retinal structure imaging was performed with high lateral resolution achieved by the modal-based wavefront sensorless algorithm. The WSAO-SD-OCT was capable of optimizing up to 12 Zernike modes, thereby allowing resolution of which was sufficient for resolving the cone mosaic in the human retina, even at small angles of eccentricity in nonmydriatic pupils. However, the narrow field of view and long optimization time (around 6 to 12 s) limited the system's suitability for clinical applications. In this work, we introduced real-time retinal tracking implemented on a GPU. Tracking the axial position of the retina in real time adds robustness to the image-based merit function, and is essential for clinical imaging. The development of hardware-based axial eye tracking has been reported by Pircher et al.<sup>38</sup> In this work, we utilize high-speed B-scan image acquisition and real-time processing to achieve retinal tracking in a software solution.

The goal of our system was to build a clinically friendly imaging system that was capable of providing high-resolution information to complement existing retinal imaging systems and glaucoma studies.<sup>17,22</sup> Thus, although our system resolution of  $\sim 4.3$   $\mu$ m was lower than the lateral resolution achievable from the previous reported WSAO-SD-OCT, we were able to acquire volumes across a relatively larger field of view with sufficiently high resolution and high speed to visualize the micro-architecture of the entire ONH. The inclusion of both high resolution and wide field of view is important for visualizing the pathological changes due to glaucoma in the ONH and in the NFL. For example, visualization of the circumpapillary nerve fibers in combination with the measurement of retinal NFL thickness has the potential to improve sensitivity and specificity in detecting glaucoma.<sup>16</sup>

We demonstrated human retinal imaging with a VL for defocus correction and dynamic focus adjustment. The lateral resolution in the retina could be further improved through the correction of low-order aberrations, such as astigmatism, in addition to defocus. Although the pupil diameter of the imaging beam used in this system is larger than that in common commercial OCT instruments in the 830-nm wavelength range, the ocular aberrations from the small sample size of subjects imaged (five people with normal eye health, and mild myopia) did not noticeably detract from the image quality. We anticipate replacing the VL element with a more sophisticated adaptive lens to build a compact system that can correct for higher-order optical aberrations using image-driven optimization.<sup>39,40</sup> For example, Liebertraut et al.<sup>41</sup> reported a flexible elastomer based tunable microlens capable of tuning astigmatism as

well as defocus. Alternatively, integrating the multiactuator adaptive lens<sup>42</sup> into the OCT system presented in this report to correct for low-order aberrations (astigmatism) would allow for a compact and simple retinal imaging system that would be suitable for translation to the clinic.

## 5 Conclusion

*En face* view of OCT stacks provides important and complementing visualizations of the retina and ONH investigating biomarkers of glaucoma preceding vision loss. We demonstrated the combination of high-performance massively parallel processing of SS-OCT volumetric data for real-time axial tracking and display. In combination with an electrically controllable VL, we demonstrated acquisition of focus-stacked OCT volumes with high resolution throughout an extended depth range.

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