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### Two-color temporal focusing multiphoton excitation imaging with tunable-wavelength excitation

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Abstract. Wavelength tunable temporal focusing multiphoton excitation microscopy (TFMPEM) is conducted to visualize optical sectioning images of multiple fluorophore-labeled specimens through the optimal two-photon excitation (TPE) of each type of fluorophore. The tunable range of excitation wavelength was determined by the groove density of the grating, the diffraction angle, the focal length of lenses, and the shifting distance of the first lens in the beam expander. Based on a consideration of the trade-off between the tunable-wavelength range and axial resolution of temporal focusing multiphoton excitation imaging, the presented system demonstrated a tunable-wavelength range from 770 to 920 nm using a diffraction grating with groove density of 830 lines/mm. TPE fluorescence imaging examination of a fluorescent thin film indicated that the width of the axial confined excitation was  $3.0 \pm 0.7 \,\mu$ m and the shifting distance of the temporal focal plane was less than 0.95  $\mu$ m within the presented wavelength tunable range. Fast different wavelength excitation and three-dimensionally rendered imaging of Hela cell mitochondria and cytoskeletons and mouse muscle fibers were demonstrated. Significantly, the proposed system can improve the quality of two-color TFMPEM images through different excitation wavelengths to obtain higher-quality fluorescent signals in multiple-fluorophore measurements. © 2017 Society of Photo-Optical Instrumentation Engineers (SPIE) [DOI: 10.1117/1.JBO.22.2.026008]

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#### Introduction 1

Multiphoton excitation (MPE) microscopy facilitates threedimensional (3-D) imaging of fluorescence-labeled molecules in in vivo biospecimens with favorable penetration depth, low invasiveness, and minimal photobleaching and photodamage.<sup>1-5</sup> Because of the requirement of fast frame rate in applications of live samples, many studies have demonstrated that the temporal resolution of MPE fluorescence imaging exhibits a great improvement when temporal focusing MPE microscopy (TFMPEM) is applied.<sup>6-12</sup> Compared with MPE fluorescence imaging that uses only spatial focusing excitation and point-by-point scanning to map the images, scanless temporal focusing directly obtains the maximal excitation probability only in the image plane through pulse propagation geometry.<sup>6-13</sup> The TFMPEM configuration functions by spatially separating the frequencies of a short pulse through a diffraction device, collimating these beams using a lens, and recombining them using an objective lens. Finally, the different frequency components are overlapped in phase at the focal plane. $^{6-8}$  This process appears to create a plane illumination that features a short, high-peak power pulse to excite the multiphoton fluorescence of specimens. Thus, by synchronizing the control signals of the axial-scanning piezo stage and electron-multiplying charge-coupled device (EMCCD), the volumetric imaging rate of TFMPEM was demonstrated to be 30 volumes/s.<sup>14</sup>

However, the lateral and axial resolutions of TFMPEM imaging that is based on a configuration of the widefield excitation are several hundred nanometers and several micrometers. The spatial resolution of TFMPEM remains a concern for

Although these improvements in temporal and spatial resolutions enable TFMPEM to be a powerful platform for visualizing the dynamic distribution of molecules and cells and the architecture of subcellular structures in biotissues, TFMPEM is insufficient for performing efficient excitation of fluorophores with different two-photon absorption spectra in multifluorophore imaging through an illuminated configuration of fixed wavelength pulse lasers. Many fluorescence proteins and fluorophores used for biomedical studies have demonstrated the specific spectra of multiphoton absorption.<sup>25-30</sup> The highly efficient MPE of fluorophores proves the superior SNR of MPE imaging, which is critical for deep imaging.<sup>31–33</sup> Although the fluorescent excitation of two different fluorophores with overlapping two-photon absorption spectra using conventional TFMPEM with a single

bioimaging applications. Structured light illumination techniques, such as nonlinear structured illumination microscopy and HiLo microscopy for TFMPEM, were developed to increase the signal-to-noise ratio (SNR) of MPE images by reducing the scattering signals from the out-of-focus fluorescence and to improve the spatial resolution of TFMPEM in turbid media.<sup>15-17</sup> The patterned illumination of TFMPEM can be created using the projection of a fringe and grid,<sup>18</sup> a spatial light modulator,<sup>19-21</sup> and a digital micromirror device (DMD).<sup>22</sup> Additionally, TFMPEM combined with astigmatism imaging can indicate the positions of fluorescent particles and molecules in 3-D with applied positioning resolution of  $\sim$ 14 nm (lateral) and 21 nm (axial). The combination can additionally extract the particles and molecule transport trajectories to explore the motion behaviors of fluorescent particles and the interaction of molecules.23,24

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excitation wavelength can be achieved, the selection of fluorophores for biomedical applications is restricted.<sup>24</sup> In spatialfocusing-only MPE microscopy using galvo scanners to map MPE fluorescence images, matching the maximum multiphoton absorption wavelength of different fluorophores is straightforward through adjustment of the incident wavelength of ultrafast pulse lasers, such as the mode-locked ultrafast Ti:sapphire pulse laser, the supercontinuum pulse laser, and the tunable ultrafast pulse fiber laser.<sup>31,34–36</sup> However, adjusting the incident wavelength of TFMPEM in real time to obtain the optimum efficiency of MPE is difficult because of the use of a diffraction device, such as an optical diffuser,<sup>37</sup> a diffraction grating,<sup>6-12,20,21,24</sup> a dualprism grating,<sup>38</sup> or a DMD,<sup>14,17,22,23</sup> which separates the frequencies of incident pulse at different diffraction angles. Therefore, TFMPEM with tunable wavelength excitation was implemented using an optical setup to automatically vary the incident angle of the ultrafast pulse light source at the diffraction grating depending on its central wavelength in this study. Moreover, the proposed system was used to visualize two-photon excitation (TPE) fluorescent section images of the Hela cell cytoskeleton and mouse muscle fibers through fast tunable-wavelength excitation. Furthermore, the intensity enhancement of a two-color TPE fluorescence image of multifluorophore-labeled specimens through optimum wavelength excitation in the fast tunablewavelength excitation TFMPEM system was demonstrated.

#### 2 Materials and Methods

#### 2.1 Sample Preparation

To fabricate a rhodamine 6G thin film, a polymethylmethacrylate solution doped with rhodamine 6G (Sigma) was spin-coated on glass cover slips at 6000 rpm for 60 s and baked in an oven at 120°C for 15 min. The thickness of the rhodamine 6G thin film was less than 200 nm.<sup>11</sup>

Mouse muscle specimens were permeabilized using 0.1%Triton X-100 in 1× phosphate-buffered saline (PBS) buffer for 10 min. After the specimens were washed three times with 1× PBS buffer, a diluted solution of Alexa Fluor 488-labeled phalloidin (Invitrogen) with a dilution of 100 was added to the specimens to stain the actin. After 2 h of incubation, the mouse muscle specimens were washed three times with a PBS solution with 0.05% Tween 20 (Sigma). The mouse muscle specimens were then used to obtain two photon fluorescence images of muscle fiber. The preparation of mouse specimens was approved by the Institutional Animal Care and Use Committee, National Central University, Taiwan.

Hela cells were seeded on cover slips using Dulbecco's modified Eagle's medium (Gibco) supplemented with 10% (v/v) fetal bovine serum that contained 1.0-mM sodium pyruvate, 0.1-mM nonessential amino acids, 1.5-g/L sodium bicarbonate, and 2-mM L-glutamine. The cells were incubated at 37°C in 5% CO<sub>2</sub>. After 24 h of incubation, some Hela cell specimens were fixed using 4% paraformaldehyde for immunofluorescence staining, and the other Hela cell specimens were retained to transfect the fluorescence protein. Hela cells were transfected with an enhanced green fluorescent protein (EGFP), which was fused with a cytoskeleton protein, actin. For the transfection process, a solution that contained 2  $\mu$ g of actin-EGFP plasmid DNA, 6 µL of lipofectamine 2000 (Thermo), and 250  $\mu$ L of Opti-MEM (Thermo) was added to the Hela cells. After 48 h of incubation, the transfected Hela cell specimens were also fixed using 4% paraformaldehyde for the subsequent immunofluorescence staining. The tubulin of Hela cells was stained using a primary antibody against tubulin (1  $\mu$ L/mL; Sigma) and 5  $\mu$ L/mL secondary antibodies labeled with Alexa Fluor 568 (Invitrogen). The mitochondria of transfected Hela cells were stained with a primary antibody against mitochondria (20  $\mu$ L/mL; Abcam) and 5  $\mu$ L/mL secondary antibodies labeled with Alexa Fluor 568. Finally, antibodies exhibiting nonspecific binding were washed out using the PBS solution.

#### 2.2 Optical System Setup

The configuration of the whole optical system setup is shown in Fig. 1(a). The excitation laser source is the mode-locked ultrafast Ti:sapphire laser (Chameleon version II, Coherent), which features a pulse width of 140 fs, a beam size of ~1.2 mm, a repetition rate of 80 MHz, and a wavelength tuning range of 680 to 1080 nm. A half-wave plate (Newport), which is mounted on the rotation stage, and a linear polarizer (Newport) are used to adjust the laser power. The power density of the excitation laser at the specimens was ~24.7 kW/cm<sup>2</sup>; such a high power density was used to ensure that the TPE fluorescence intensity of the fluorophores at each excitation wavelength was adequate for recording the wavelength response of the TPE fluorescence intensity of fluorophores. For imaging, the power density at the specimens labeled using Alexa Fluor 568 can be decreased to  $4 \text{ kW/cm}^2$  through the optimum wavelength excitation of fluorophores. The excitation light passes through the beam expander and tunes the propagation angle of light for the excitation wavelengths from 770 to 920 nm as shown in Fig. 1(b). A detailed description of the variation of the propagation angle of light follows in Sec. 2.3. The first-order diffraction light is generated by illumination on an 830-lines/mm grating at the same position for different wavelengths. Consequently, the light passes through a 4f lens system and an upright optical microscope (Olympus) combined with a water-immersion objective (60× PlanApo, Olympus) featuring a numerical aperture of 1.2 to excite the fluorescence signal of specimens. The fluorescence signals of the multiphoton images were collected for the same objective and reflected by a multiphoton single-edge dichroic beamsplitter (FF705-Di01-25x36, Semrock). After the fluorescence signal passed through an imaging lens (f = 200 mm, Thorlabs), the signal was filtered using an emission filter wheel featuring two bandpass filters (FF01-525/45-25 and FF01-585/ 40-25, semrock) and imaged on an EMCCD camera (iXon Ultra 897, Andor). To obtain 3-D images, the specimen was moved along the z-axis using a motorized focus stage (Prior Scientific). These motion devices were all synchronized with a data acquisition card and a custom LabVIEW program interface, which controlled the center wavelength of the excitation light, the shutter, the rotation stage (Newport) for adjusting laser power, the linear motion stage (Throlabs) for varying the incident angle of light on the grating, the filter wheel for changing the emission filter, the motorized focus stage, and the EMCCD cameras for capturing the sequential section multiphoton fluorescence images at different depths and excitation wavelengths. The system can record 3-D image stacks at each excitation wavelength, and the excitation wavelength-scanned image stacks at the same z position.

#### 2.3 Design of the Tunable Wavelength in the Imaging System

In TFMPEM, the excitation light is diffracted by the diffraction component and illuminated on the sample plane after passing



**Fig. 1** (a) Configuration of the optical system. (b) Setup of the optical system for tuning the propagation angle of light with the excitation wavelengths from 770 to 920 nm.

thorough the collimating and objective lenses of a 4f system. The spatially separated excitation lights, after passing through the diffraction component, must be recombined and in phase at the focal plane of objective lens to excite multiphoton fluorescence, and the diffracted light of the center frequency of the light source follows the optical axis of the 4f system. To implement TFMPEM with the capability of fast excitation wavelength tuning, the optical components should be moved to ensure that the diffracted light of the center frequency of the light source can follow the optical axis of the following 4f system because the diffraction angle is a function of the wavelength of the excitation light. This can be achieved through two general approaches: (1) rotate the optical axis of the 4f system according to the central frequency of the light source or (2) rotate the diffracted light according to the fixed optical axis of the 4f system. The first approach is complicated because the collimating lens and all components of the microscope, including the dichroic mirror, objective lens, specimen, and camera, must be rotated. In the second approach, the diffraction component can be mounted on a rotation stage and rotated to ensure that the diffracted light is along the fixed optical axis of the 4f system. However, the illumination plane of the recombined excitation lights is conjugated to the diffraction plane of the diffraction component; therefore, rotating the diffraction component induces a tilt angle between the illumination plane of the recombined excitation lights and the focal plane of the objective lens. This approach causes mismatch between the excitation plane of the TPE and the collection plane of the objective lens. An alternative method is to rotate the incident angle on the fixed diffraction component to ensure that the diffraction angle is along the fixed optical axis of the 4f system. In this approach, the region projected on the fixed diffraction component must be the same for different wavelengths because it conjugates with the excitation plane. Accordingly, we developed an optical system in which a motorized linear stage is combined with a beam expander to adjust the angle of incidence on the diffraction device in TFMPEM. The mechanism of the optical system that adjusts the propagation angle of light for different excitation wavelengths was demonstrated [Fig. 1(b)]. The following concerns were considered for the selection of optical devices in the proposed TFMPEM. First, the diffraction component of a temporal focusing system can be utilized to diffract the frequencies of excitation light at different spatial angles. In this study, we used the grating as the diffraction component. The different frequencies of excitation light were recombined and overlapped in phase at the focal plane. The plane area for the MPE can be obtained through temporal focusing. Consequentially, the excitation light in the proposed TFMPEM was considered for different central wavelengths. On the basis of the concept of the temporal focusing system, the incident angle on the diffraction device plays an important role for the fast tuning excitation wavelength. The diffraction equation of the grating can be expressed as<sup>39</sup>

$$m\lambda = a(\sin\,\theta_{\rm i} + \sin\,\theta_m),\tag{1}$$

where *m* is an integer and the diffraction order,  $\lambda$  is the central wavelength of the ultrafast laser, *a* is the effective pitch of the grating,  $\theta_i$  is the incident angle, and  $\theta_m$  is the diffraction angle at the *m*'th-order diffraction. In the setup of the proposed system, the direction of the first-order diffracted light (*m* = 1) is set at 0 deg (i.e.,  $\theta 1 = 0$  deg) to ensure that the beam is spatially dispersed with the central frequency traveling along the optical axis of the following 4f system despite changes in wavelength. The incident angle  $\theta_i$  must be adjusted for the diffraction equation, and the incident angle is rewritten as

$$\theta_{\rm i}(\lambda) = \sin^{-1}\left(\frac{\lambda}{a}\right).$$
(2)

For the different groove densities of the grating, the incident angle at the central wavelengths from 700 to 1000 nm is shown in Fig. 2(a). The results indicated that the incident angle increased as the groove density increased. The incident angle for the groove densities of 600 and 830 (lines/mm) was from 24.8 deg to 36.9 deg and from 35.2 deg to 56.1 deg at the central wavelengths from 700 to 1000 nm, respectively. The case of a 1200 lines/mm grating does not cover all the central wavelengths; there is only a small tunable range of the central

wavelength, which is from 700 to 835 nm. Moreover, the axial resolution of TFMPEM can be expressed as<sup>40,41</sup>

$$\text{FWHM}_{\text{axial}} \propto 2\sqrt{3}Z_{\text{R}} = 2\sqrt{3} \left[ \frac{2f_{\text{obj}}^2}{k_o(s^2 + \alpha^2 \Omega^2)} \right], \tag{3}$$

where  $Z_{\rm R}$  is the Rayleigh length of the focused spatially chirped beam,  $f_{\rm obj}$  is the focal length of the objective,  $k_o$  is wavevector, sand  $\alpha \Omega$  are the monochromatic and full frequency spectrum spot sizes at the back focal plane of the objective. The constant  $\alpha$  is proportional to the focal length of the collimating lens and the groove density of grating. Assume that the focal length of the collimating lens is constant. According to Eq. (3), the higher groove density of grating increases the value of  $\alpha$  to provide the better confinement of axial excitation. Considering a trade-off between the tunable wavelength range and axial resolution of TFMPEM, the groove density of 830 (lines/mm) is used in this study.

Second, the excitation beam should illuminate the same position on the grating for the different wavelengths with their specific incident angles according to the preceding calculation. Thus, the grating is placed at the focal plane of the second lens of the beam expander in the optical system. The collimated expanded beam could illuminate the grating at a specific incident angle after it passed the second lens, when the focusing position of the first lens demonstrates a small shift, as shown



**Fig. 2** (a) Incident angles for the different central wavelengths of the laser for maintaining the first-order diffracted light with a diffraction angle of 0 deg for three conditions of the groove density of the grating. (b) Variation of the incident angle of the light source on the grating as a function of the shift of the focusing position of the first lens for three focal lengths of the second lens. (c) Simulated light propagation path for the excitation wavelengths from 770 to 920 nm.

in Fig. 1(b). Here, the incident angle of the excitation beam on the grating could be varied by controlling the shift of the first lens and maintaining the same illuminated position and diffraction angle on the grating for the different central wavelengths. Third, the variation amount of the incident angle caused by the shift of this focusing position was evaluated. The relation between the angle change,  $\phi$ , of the output beam of the second lens and the shifting position, *d*, of the first lens is expressed as

$$\phi = \sin^{-1}(d/f_2),\tag{4}$$

where  $f_2$  is the focal length of the second lens of the beam expander. Figure 2(b) shows that the amounts of angle change were 14.48 deg, 9.59 deg, and 7.18 deg after the first lens with a focal length of 40 mm was shifted to a focusing position of 25 mm for focal lengths of the second lens of 100, 150, and 200 mm, respectively. In our practice system, the initial settings of the excitation light were a central wavelength of 920 nm and alignment along the optical axis with the incident angle of  $\theta_c$  as shown in Fig. 1(b). Furthermore, by combining Eqs. (2) and (4), the shifting distant for a central wavelength,  $\lambda_i$ , could be expressed as

$$d = f_2 \sin[\sin^{-1}(\lambda_i/a) - \sin^{-1}(920 \text{ nm}/a)]$$
  
=  $f_2 \sin[\sin^{-1}(\lambda_i/a) - \theta_C].$  (5)

We considered a laser with an initial beam size of 3 mm that passed through the first lens with a focal length of 40 mm. Moreover, we assumed that the second lens had a focal length and diameter of 100 and 50 mm, respectively. The divergence angle of the beam between the focusing positions of the first lens and the second lens was estimated at 2.147 deg. The maximum acceptable shift of the first lens on the motion stage was then determined. Furthermore, the optical path for an 830-lines/ mm grating was simulated [Fig. 2(c)]. The presented optical system, which eliminates the mismatch between the excitation plane of the TPE and the collection plane of the objective lens, illuminates the same illumination position on the grating for different wavelengths. It uses a simple approach wherein the shift of the first lens of the beam expander is controlled for TFMPEM with excitation wavelength tuning. Moreover, the maximum and minimum efficiencies of the excitation light

diffracted through the diffraction grating in the excitation wavelength tuning system were 65% and 59.6%, respectively, as the wavelength was varied from 770 to 920 nm. This tendency is consistent with the grating specifications. Therefore, the excitation power necessary to illuminate the specimens can be maintained by rotating the half-wave plate to adjust the incident power at each wavelength according to the characteristic efficiency of the diffraction grating. Thus, TFMPEM with a tunable wavelength range from 770 to 920 nm and the same illuminated position on the 830-lines/mm grating was demonstrated.

#### 3 Experimental Results and Discussion

#### **3.1** Axial Resolution at Different Excitation Wavelengths

To determine the capability of axial sectioning at different wavelengths, a rhodamine 6G thin film with a thickness of less than 200 nm was examined. For temporal focusing excitation with wavelength scanning, the system was capable of axial sectioning and providing the same excited plane of the specimen at d ifferent laser wavelengths. Here, the rhodamine 6G thin film was axially scanned with a range of 40  $\mu$ m and a step size of 0.5  $\mu$ m using the motorized focus stage. Figure 3(a) shows the axial intensity profiles of TPE fluorescence of the rhodamine 6G thin film with the excitation wavelengths from 770 to 920 nm and a wavelength shift of 50 nm.

Examination of the full width at half maximum of the normalized intensity profile revealed that the width of axial confined excitation was  $3.0 \pm 0.7 \,\mu m$  for this wavelength range. This finding indicates that TFMPEM has axial sectioning capability at each wavelength. As shown in the axial intensity profiles in Fig. 3(a), we extracted the peak position of the intensity profile to determine the position of the focal plane at every excitation wavelength. The amount of axial shifting of the temporal focal plane at the different wavelengths is illustrated in Fig. 3(b). On the basis of a previous study, the temporal focal plane can be shifted axially by tuning the group velocity dispersion in the excitation path.9 Consequently, the variation in the temporal focal plane may be induced by the group velocity dispersion effect of the system. However, the shift of the temporal focal plane was less than 0.95  $\mu$ m. Therefore, the system provides the capability to illuminate the same excitation



**Fig. 3** (a) Axial normalized TPE fluorescence intensity profiles of the thin fluorescent film with excitation wavelengths from 770 to 920 nm and a wavelength shift of 10 nm. (b) Axial shift of the temporal focal plane position at the different wavelengths.



**Fig. 4** Widefield TPE fluorescence images of the muscle fibers stained with Alexa Fluor 488-labeled phalloidin at (a) different excitation wavelengths, (b) different depths with an excitation wavelength of 770 nm. (c) The fluorescence intensity profiles of the Hela cell tubules stained with Alexa Fluor 568 along the yellow dashed line of inset image for the different excitation wavelengths. Scale bars, 15  $\mu$ m.

area at a specific section within the specimen and to achieve wavelength-scanned excitation.

#### **3.2** Two-Photon Fluorescence Images with the Multiple-Wavelength Excitation

We first present the multiple-wavelength excitation for TFMPEM in TPE fluorescence imaging of the mouse muscle fibers stained with Alexa Fluor 488-labeled phalloidin. Figure 4(a) illustrates the optical section imaging results at the same depth of mouse muscle fibers at every excitation wavelength with a wavelength shift of 20 nm in a wavelength range from 770 to 920 nm. The image intensities shown in Fig. 4(a) are the raw values of the fluorescence signals. For clarity, the contrast of the insets in the results for the excitation wavelengths from 810 to 910 nm in Fig. 4(a) was enhanced by approximately ninefold to reveal differences in morphology. The results indicated that the maximum fluorescence intensity and more favorable contrast of the mouse muscle fiber images were achieved using the excitation wavelength of 770 nm. Thus, to obtain higher quality in 3-D imaging, the excitation wavelength of 770 nm was used. The section images of the mouse muscle fibers at every z position with a step shift of 1  $\mu$ m for visualizing their morphology and distribution are shown in Fig. 4(b). Moreover, TPE fluorescence images of the Hela cell tubules labeled using Alexa Fluor 568 were captured at different excitation wavelengths. The maximum excitation efficiency of TPE



Fig. 5 Section TPE fluorescence images of mitochondria (red) and actin filaments (green) of Hela cells with TPE wavelengths from 770 to 920 nm and a wavelength shift of 10 nm. The mitochondria and actin filaments were labeled with Alexa Fluor 568 and EGFP. Scale bar, 15  $\mu$ m.



**Fig. 6** Merged TPE fluorescence images of mitochondria (red) and actin filaments (green) (a) with an excitation wavelength of 820 nm and (b) with an excitation wavelength of 790 nm for mitochondria and with an excitation wavelength of 900 nm for actin filaments in Hela cells. (c) Bright field image. Scale bar, 15  $\mu$ m.

fluorescence was realized at an excitation wavelength of 790 nm, as shown in the inset of Fig. 4(c). Furthermore, Fig. 4(c) presents the intensity profiles of the TPE fluorescence signals along the yellow dashed line in the inset. Comparison of the intensity profiles through the different excitation wavelengths shows that the proposed system provides an approach that improves the contrast of TFMPEM images by selecting the optimized excitation wavelength to match the superior excitation efficiency of fluorophores.

#### **3.3** Intensity Enhancement of TPE Fluorescence Images of Two Types of Fluorophore-Labeled Specimens by Wavelength Selection Excitation

To demonstrate the capacity of the proposed TFMPEM system for improving the quality of images in multifluorophore-labeled specimen measurements using wavelength selection excitation, the system was used to visualize the TPE fluorescence images of the mitochondria stained with Alexa Fluor 568 and the actin filaments labeled with EGFP in Hela cells. Figure 5 illustrates the merged section images of the mitochondria (labeled red) and the actin filaments (labeled green) at every excitation wavelength with a wavelength shift of 10 nm in a wavelength range from 770 to 920 nm. These fluorescence data of mitochondria



Fig. 7 Normalized TPE fluorescence intensity as a function of the excitation wavelength for the muscle fibers stained with Alexa Fluor 488, the mitochondria stained with Alexa Fluor 568, and the actin filaments labeled with EGFP.

and actin were recorded with exposure times of 0.1 and 4 s by switching the emission filter in front of the camera at every excitation wavelength. The fluorescence intensity of the mitochondria is clearly superior at an excitation wavelength of 790 nm, but the fluorescence intensity of the actin filaments is superior at an excitation wavelength of 900 nm. The excitation wavelength of the conventional TFMPEM system with a fixed single excitation wavelength for revealing the morphology of the mitochondria and actin filaments with the barely acceptable intensity of two labeled fluorophores simultaneously is 820 nm in Fig. 6(a). To acquire high-contrast merged images, the other approach using our TFMPEM system is shown in Fig. 6(b). On the basis of the results illustrated in Fig. 5, the maximum signals of TPE fluorescence images for the mitochondria with an excitation wavelength of 790 nm and actin filaments with an excitation wavelength of 900 nm are shown in Fig. 6(b). Accordingly, higher-quality merged TPE fluorescence images of the mitochondria and actin filaments can be obtained using wavelength selection excitation. Additionally, according to Figs. 4(a) and 5, the normalized TPE fluorescence intensity of Alexa Fluor 488, Alexa Fluor 568, and EGFP from the TPE fluorescence images of the muscle fibers, the mitochondria, and the actin filaments with excitation wavelengths from 770 to 920 nm was determined as shown in Fig. 7. The results indicate that the wavelength response of the normalized TPE fluorescence intensity of fluorophores is similar to that of the twophoton absorption of fluorophores in previous works.<sup>29,42–44</sup>

#### 4 Conclusions

A proposed approach for fast wavelength scanning TFMPEM imaging can successfully obtain multiwavelength-excited and 3-D rendered fluorescence images of fluorescence-labeled biosamples. We present an approach for achieving fast TFMPEM wavelength scanning. The ultrafast pulse source with different central wavelengths generated from the mode-locked ultrafast Ti:sapphire laser changed the illuminated angle and maintained the same illumination position and diffraction angle on the diffraction grating to enable maintaining the same optical path after passing through the diffraction grating. Furthermore, the tunable-wavelength range, which depended on the groove density of the grating, the diffraction angle, the focal length of lenses, and the shifting distance of the first lens, was estimated. Because of the trade-off between the tunable-wavelength range and axial resolution of temporal focusing MPE imaging, a wavelength scanning range from 770 to 920 nm was implemented in this

study. Moreover, a width of the axial confined excitation of  $3.0 \pm 0.7 \ \mu m$  and a shifting distance of the temporal focal plane of less than 0.95  $\mu m$  were demonstrated. In TFMPEM imaging of the Hela cell mitochondria and cytoskeleton and mouse muscle fibers, the proposed system can achieve the fast different wavelength excitation and 3-D imaging. The results of wavelength scanning excitation in multifluorophore-labeled specimen measurement show that the proposed system provides an approach for enhancing the fluorescent signals and improving the imaging quality of two-color TFMPEM by exciting the wavelength with the maximum TPE of different fluorophores compared with conventional TFMPEM with a fixed single-wavelength excitation. This presented system is useful for the fast multicolor imaging of temporal focusing MPE microscope in multifluorophore-labeled biosamples.

#### Disclosures

The authors declare no competing financial interest.

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Biographies for the authors are not available.